Design of a New Honeycomb PCF for Ultraflatten Dispersion over Wideband Communication System

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ABSTRACT
A new kind of honeycomb photonic crystal fiber structure with triangular lattice is proposed. For the proposed design three different air-hole diameters in cladding region is used. To calculate dispersion, 2-D finite difference frequency domain method with the Transparent Boundary conditions (TBC) absorbing boundary conditions is used. Through the numerical simulation and optimizing the geometrical parameters like changing the diameter of air holes (d) for photonic crystal fibers in triangular lattice structure, it has been demonstrated that it is possible to obtain ultra flatten dispersion over a wide wavelength range which lies in second and third telecom window. The ultra flatten dispersion ±0.13 is obtained in the wavelength range 1.4 to 1.71 μm. The proposed structure is designed using seven ring in which circular air holes are used. The best choice of material for the designing purpose is silica with refractive index 1.458.

Keywords
Effective Refractive Index (n_eff), Photonic Crystal Fiber (PCF), Transparent Boundary Condition (TBC).

1. INTRODUCTION
As the elegant propagation properties, photonic crystal fibers (PCFs) have engrossed right smart consideration since the first fabrication of PCF in the year of 1996 [1]. Now days several analysis teams are creating constant effort all over the world to determine prevalence of PCFs over conventional fibers due to its novel optical characteristics. It has been reported that PCF will notice as endlessly single-mode guiding fiber [1], manageable nonlinearity [2] and the chromatic dispersion [1]-[8] etc over the large wavelength range.

Several designs for the PCFs have been proposed to achieve nearly zero ultra-flattened chromatic dispersion properties. PCFs with two-defected air hole rings [3], nonlinear PCFs with several kinds of air hole diameters [4], a modified hexagonal PCFs [5] and square PCFs [6] have been proposed. Some of the design procedure becomes complicated to achieve nearly zero ultra-flattened dispersion.

Recently honeycomb [7] PCFs with four kinds of air hole diameters with ultra-flattened dispersion for seven rings was proposed. However, many previous designs are all based on triangular PCFs [1], [3], [5] (see Figure 1), ultra-flattened dispersion properties of square-lattice PCFs [6] (see Figure 2) and a few reports on ultra-flattened dispersion properties of honeycomb PCFs [8], [9], [11]. A few designs were proposed on honeycomb PCF. These designs do not have better dispersion as compare to other design so it is very necessary to investigate ultra-flattened dispersion in honeycomb PCFs.

Now days, exploiting multiple design parameters such as diameter of air holes, shape of the holes (like circular, square, elliptical) and pitch difference, using different kinds of available materials like silica [1]-[5], [7]-[9], As2Se3, borosilicate crown glass [10], [12] etc., the number of air hole rings and the spacing between these holes facilitates development of PCFs with improved properties.

In this research numerically investigated and proposed a new type of honeycomb Photonic crystal fiber. According to proposed structure, it is possible to design a honeycomb PCFs with nearly zero ultra-flattened chromatic dispersion over second and third optical window by optimizing only three geometrical parameters for air hole diameters as well as a constant pitch (Λ).

For the designing purpose, used a full vector analysis based method on the finite difference time domain (FDTD) method to analyze the various properties of PCFs. Transparent Boundary conditions (TBC) absorbing boundary are positioned outside the outermost of proposed design. Numerical results shown that the PCFs has nearly zero ultra-flattened chromatic dispersion of ±0.13 ps/(nm·km) in all C
The geometrical dispersion (known as
\[ D = \frac{1}{c} \frac{d^2}{d\lambda^2}[\Delta(n_{eff})] \] (1)
where Re \( n_{\text{eff}} \) is the real part of \( n_{\text{eff}} \), \( \lambda \) is wavelength, and \( c \) is the velocity of light in vacuum.
The total dispersion is determined by the sum of the geometrical dispersion (known as waveguide dispersion) and the material dispersion obtained as shown in eq. 2 [1, 5]:
\[ D(\lambda) = D_g(\lambda) + \Gamma D_m(\lambda) \] (2)

where \( D_g(\lambda) \) and \( D_m(\lambda) \) are the geometrical and material dispersions, respectively.

The PCF structure works in optical transmission media with zero dispersion and uniform response in different wavelength range. The PCF is having so many unique properties such as high birefringence [1], [6], high nonlinearity [2], [4], wideband dispersion flattened characteristics [1]-[4], [6]-[8], endlessly single mode guiding [1], [2], [6] so that they are widely used in fiber sensors application [1] and fiber lasers as well as supercontinuum generation [10], nonlinear optics [2], [4], telecommunications, soliton [2], medical instrumentations [9] and many more application which are not realizable by conventional optical fiber.

The effects that are contributed to attenuation as well as dispersion depend on the optical wavelength. There are various wavelength bands or windows. In these windows effects are sluggish and these are the maximum positive for transmission. All windows have been regulated and currently characterized bands are the following (see Table 1) [14]

<table>
<thead>
<tr>
<th>Band</th>
<th>Description</th>
<th>Wavelength Range</th>
</tr>
</thead>
<tbody>
<tr>
<td>O band</td>
<td>Original</td>
<td>1260 to 1360 nm</td>
</tr>
<tr>
<td>E band</td>
<td>Extended</td>
<td>1360 to 1460 nm</td>
</tr>
<tr>
<td>S band</td>
<td>Short wavelengths</td>
<td>1460 to 1530 nm</td>
</tr>
<tr>
<td>C band</td>
<td>Conventional Wavelength</td>
<td>1530 to 1565 nm</td>
</tr>
<tr>
<td>L band</td>
<td>Long Wavelengths</td>
<td>1565 to 1625 nm</td>
</tr>
<tr>
<td>U band</td>
<td>Ultra long Wavelengths</td>
<td>1625 to 1675 nm</td>
</tr>
</tbody>
</table>

The minimal attenuation occurs at 1.55 \( \mu \)m wavelength in silica glass, while the minimum material dispersion reported at 1.312 \( \mu \)m wavelength [14]. The preference is occupying on short wavelengths which affects the signal is known as delay distortion. For example, creates the expanding in transmitted light pulses so that it will cause restriction of the information carrying capacity fiber. Therefore, it becomes necessary to investigate the dispersion properties of an optical fiber especially for Photonic Crystal Fiber.
Where $f$ is the confinement factor in $\mu m$, which is close to unity for the most practical PCFs as the modal power is almost confined in the material with high refractive index. $D_w(\lambda)$ and $D_m(\lambda)$ are waveguide and material dispersion. The waveguide dispersion is depends upon the structure with different air holes diameter as well as pitch but the calculation of material dispersion is done by sellmeier equation as given below [12]

$$n = \sqrt{1 + \frac{\lambda_1^2}{\lambda^2\lambda_1^2} + \frac{\lambda_2^2}{\lambda^2\lambda_2^2} + \frac{\lambda_3^2}{\lambda^2\lambda_3^2}}$$

(3)

Where $\lambda = \text{Operating wavelength in} \mu m$ and the Sellmeier coefficients for Fused silica (fluorine-doped silica 1 mole \%) Sellmeier constants are:

$A_1 = 0.696166300, A_2 = 0.407942600, A_3 = 0.898479000$

$\lambda_1 = 4.67914826x10^{-3} \mu m^2, \lambda_2 = 1.35120631x10^{-5} \mu m^2,$

$\lambda_3 = 97.9340025 \mu m^2.$

4. PROPOSED DESIGN SIMULATION AND RESULT

The proposed honeycomb PCF (see Figure 4) is made up of silica glass and has an array of air holes running along its length.

![Fig 4: Air-hole distribution of the Proposed honeycomb Structure of Design-5](image)

Now here analysis of the dispersion properties for photonic crystal fiber is to be done. The designed PCF consists of a solid core with a regular array of air holes running along the length of the fiber acting as the cladding.

For the entire configurations analyzed the mean cladding refractive index is lower than the core index. The core material is silica glass which refractive index is 1.458 and the refractive index of cladding air holes is 1. The lattice structure is in triangular lattice and its structure is honeycomb structure.

Figure 5 shows the effect of changing outer holes diameter $d_1$, and other air holes diameter $d_1$ and $d_2$ is constant as .67 $\mu m$ and .705 $\mu m$ on the chromatic dispersion behavior. The outer holes diameter is 1.20 $\mu m$, 1.446 $\mu m$, 1.60 $\mu m$ for the following design-1, design-2 and design-3. The pitch is 1.8 $\mu m$ constant for all the designs. Also it can be observed that an increase or decrease of the diameter causes the dispersion parameter to increase or decrease. This has been observed that the dispersion curves are influence of the diameter of holes.

![Fig 5: Effective of varying $d_1$ diameter while keeping diameter $d_1$, $d_2$ and pitch constant](image)

Figure 6 shows the effect of varying the pitch on behavior of chromatic dispersion while keeping the entire diameter constant. The diameters are $d_1=.67$ $\mu m$, $d_2=.705$ $\mu m$, $d_3=1.446$ $\mu m$ is constant but pitch is varied 1.6 $\mu m$, 1.65 $\mu m$, 1.7 $\mu m$, 1.85 $\mu m$ from design-4 to design-7.

![Fig 6: Effective of varying the pitch while keeping diameter $d_1$, $d_2$ and $d_3$ constant](image)

Also it can be observed that an increase and decrease of pitch causes the dispersion to increase and decrease. The dispersion curves are mainly under the influence of the pitch.

All the result in figures 5 and figure 6 represents the chromatic dispersion as a function of wavelength for the seven rings honeycomb PCFs structure.

In the proposed work there is a comparison between all the seven designs is based on total dispersion (see Figure 5 and Figure 6). For above all the Design-1 to Design-7, it can conclude that Design-5 gives more flatten dispersion for a wide wavelength range as compare to other designs. The typical variation of these design parameters will result in a change of the chromatic dispersion curve nearly zero ultra-flattened chromatic dispersion between ±0.13 ps/(nm.km) for the wavelength range 1.4 $\mu m$ to 1.71 $\mu m$.

Here note that in figure 4 the total air holes area is kept constant as according to the reference paper [7]. Here it can be seen that the effect of varying the diameter of all the rings on dispersion behavior while keeping the total air holes area constant.

![Table: Comparison of various properties of proposed PCF with reference papers](image)

<table>
<thead>
<tr>
<th>PCF</th>
<th>Wavelength Range</th>
<th>Dispersion (ps/ (km-nm))</th>
<th>Flat Band (nm)</th>
<th>$N_r$, $N_a$, $N_d$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ref. [2]</td>
<td>1.30 to 1.60 $\mu m$</td>
<td>0 ± 0.6</td>
<td>300</td>
<td>5,2,3</td>
</tr>
</tbody>
</table>
At the Final, there is a comparison between various properties of the PCFs for telecom and nonlinear optics applications. Therefore, the proposed fiber with a modest number of design parameters, near-zero ultra-flattened dispersion may pave the way for various applications in optics. Table 2 shows the comparison of those fibers taking into flat dispersion, wavelength range and number of design parameters including like number of rings (N₀), number of pitch (N₁) and number of different diameter of holes (N₂) which are used in PCF design respectively.

5. CONCLUSION

A new honeycomb index guiding PCFs is numerically investigated ad proposed. The proposed honeycomb PCFs has flattened zero dispersion over a wide wavelength range. In comparison with several other previously research work presented on dispersion-flattened PCFs, the design procedure for this proposed structure would be more efficient and easier because relatively minimized geometrical parameters are required to be optimized and simple for fabrications because of considering less number of air holes. It has been shown that the proposal of honeycomb index-guiding PCFs has nearly zero ultra-flattened chromatic dispersion of 0±0.13ps/(nm·km) in second and third optical window.

As the final conclusion of this research work, the honeycomb PCFs may be suitable for chromatic dispersion management applications as a chromatic dispersion controller, dispersion compensator or as a nonlinear optical system.

6. REFERENCES


