

Three-Phase Split-Source Inverter (SSI)

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ABSTRACT

Several applications that depend on electrical DC-AC conversion sometimes need the AC output voltage to be higher than the input voltage. In case of use the traditional voltage source inverter (VSI) an additional DC-DC boosting stage is required. For this reason the single-stage DC-AC power converters are recently gaining higher attention due to their merits compared to the two-stage equivalent in terms of size, cost, weight, and complexity. They are also less complex in nature. Different impedance network converters are used in this field such as Z-source inverter (ZSI), the buck-boost voltage source inverter (BBVSI), and the Y-source inverter (YSI). In this paper another single-stage DC-AC power converter, called the split-source inverter (SSI) which has some features that is not exist in other topologies, the important one being the possibility to use the conventional modulation that used with the traditional voltage source inverter (VSI) without any modification. Here sinusoidal PWM (SPWM) and Third Harmonic Injected PWM (THPWM) are used and compared. The analysis of (SSI) has been verified by simulation. The simulation is done in MATLAB/SIMULINK.

General Terms

DC-AC, pulse-width modulation (PWM), single-stage, split-source inverter (SSI), voltage-source inverter (VSI), Z-source inverter (ZSI), Y-source inverter (YSI).

Keywords

Split-source inverter (SSI), SPWM, THPWM.

1. INTRODUCTION

Voltage source inverter (VSI) is The most popular DC- AC power converter that used in power electronic systems but its buck capability .Since the VSI can only be used as a buck inverter; the output AC makes the need to an additional DC-DC boosting stage for several applications which needs a high AC voltage exceed the available DC input voltage. It is not a matter for many applications with high DC rail, but more important for the applications require higher output AC voltage than input DC voltage such as fuel-cell based systems and renewable energy systems. So to decrease the cost, complexity, size and weight the additional boosting stage must be eliminated by using single-stage DC-AC converters which have the buck-boost capability in a one stage. This research focuses on most popular and common single-stage DC-AC power converters such as the conventional Z-source inverter(ZSI),the buck-boost voltage source inverter (BBVSI), and the Y-source inverter (YSI) shown in Fig. 1 [1]-[3]. As shown in fig.1 The (ZSI) and (YSI) have a huge impedance networks between the source and the inverter bridge. BBVSI suffers from utilizing an additional semiconductor switch in its circuit. Many other inverter topologies that are derived from ZSI or impedance fed inverter. Most of them are

reviewed in [4], but their different modulation techniques are reviewed in [5]. As seen in fig.1 all of these topologies have discontinuous input current and an oscillated voltage cross the inverter bridge, which is between zero and a controlled value.

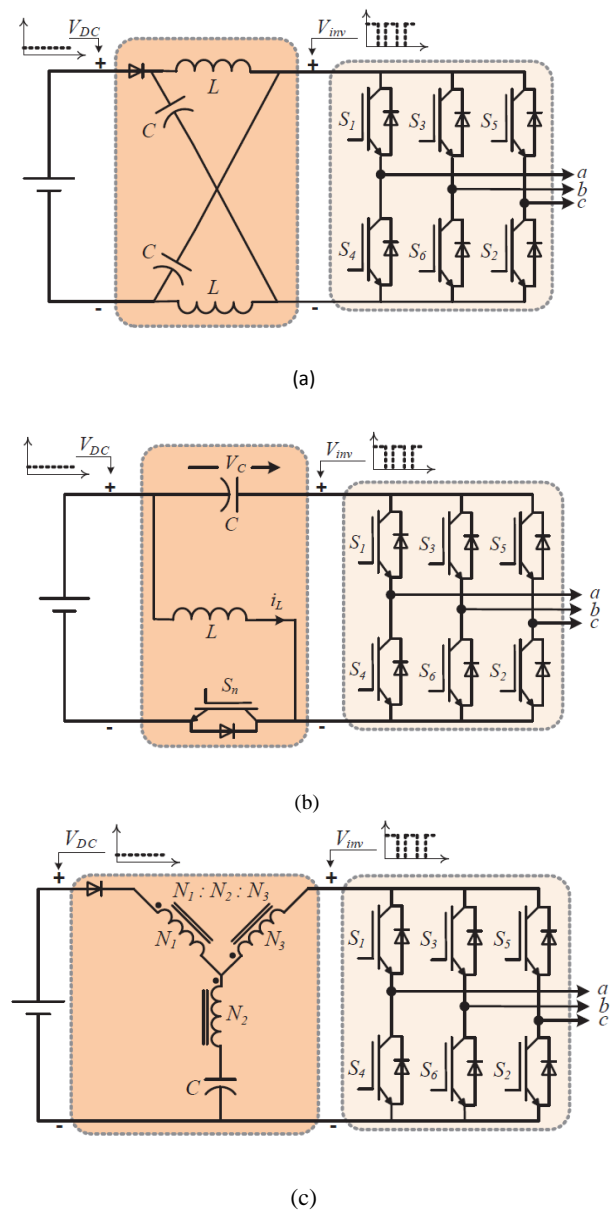


Fig.1: Common single-stage DC-AC power converters (a) Z-source inverter (ZSI) (b) Buck-boost voltage source inverter (BBVSI) (c) Y-source inverter (YSI).

Split-source inverter (SSI), shown in Fig. 2. This topology utilizes a reduced number of passive elements compared to the ZSI and the YSI, in addition it uses an additional three diodes compared to the BBVSI that uses an additional active semiconductor switch [4], [5]. The voltage across the bridge of the SSI is constant unlike the above topologies, utilizing the states of the voltage source inverter (VSI) with the conventional modulation schemes. It is combination of the boost converter with the three-phase VSI by connecting the input inductor to the split points of the B6- Bridge via diodes that prevent the capacitor discharging. Thus it is a boost inverter. SSI uses the same states of VSI, so the same modulation schemes are applied. Here sinusoidal PWM (SPWM) and third harmonic injected PWM (THPWM) are used and compared.

2. SPLIT-SOURCE INVERTER (SSI) OPERATION, MODULATION, AND MATHEMATICAL DERIVATION

2.1 SSI Operation

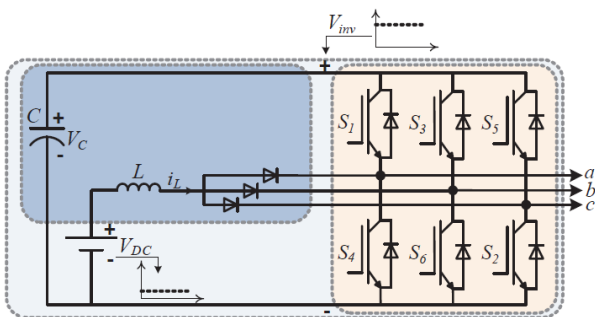


Fig.2: Split-source inverter (SSI).

The three-phase SSI, shown in Fig. 2, uses the same B6-bridge of the traditional three-phase VSI and the same eight states (000,001,...,111).When at least one of the lower switches S2, S4, and S6 is ON the inductor L gets charged. During 111 state only the upper switches is ON the inductor, L will be discharged and charge the DC link capacitor C via the freewheeling diodes [6].

2.2 SSI Modulation

The three phase split-source inverter SSI can use the conventional modulation schemes of the VSI.Here the sinusoidal pules width modulation (SPWM) and the third-harmonic injected pulse width modulation (THPWM) schemes are used and compared. The reference and carrier signals for the two schemes (SPWM) and the (THPWM) are shown in Fig. 3[6].

2.3 SSI Mathematical Derivation

The duty cycle ratio D at which the inductor L of the SSI is charged can be calculated by (1) for the SPWM and the THPWM schemes respectively. Depending on (1) and Fig. 3; the duty cycle D is not constant, it varies with a low frequency equals to three times the fundamental frequency in SPWM. This variation is small in the case of the THPWM scheme compared to the SPWM scheme [6] - [10].

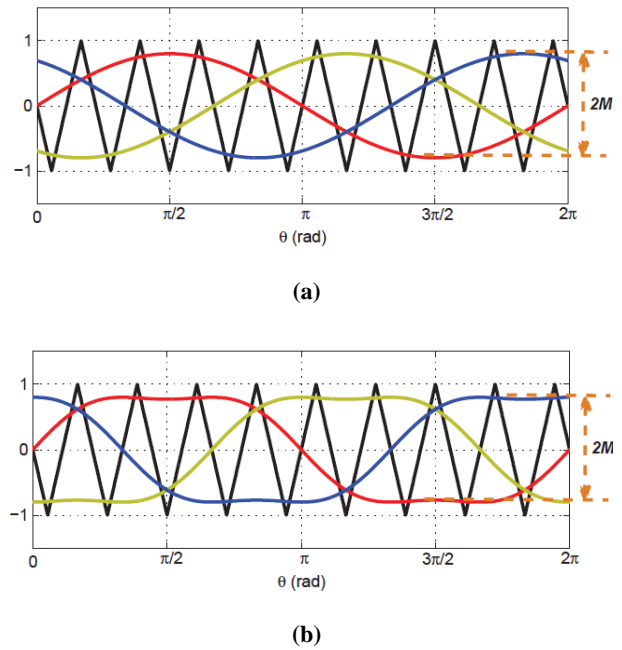


Fig.3: Employed modulation schemes reference and carrier signals (a) Using the SPWM scheme (b) Using the THPWM scheme with a third-harmonic component of 1/6 of the fundamental component.

$$D(\theta) = 0.5 - \frac{M}{2} \sin(\theta) \quad \text{SPWM}$$

$$D(\theta) = 0.5 - \frac{M}{\sqrt{3}} \left\{ \sin(\theta) + \frac{1}{6} \sin(3\theta) \right\} \quad \text{THPWM (1)}$$

Where $7\pi/6 \leq \theta \leq 11\pi/6$, and M is modulation index shown in Fig. 3. The inductor is charged with an average duty cycle D_{av} given by (2):

$$D_{av} = 0.5 + \frac{3\sqrt{3}}{4\pi} M \quad \text{SPWM}$$

$$D_{av} = 0.5 + \frac{3}{2\pi} M \quad \text{THPWM} \quad \dots (2)$$

Thus capacitor voltage VC and the inverter voltage V_{inv} will be as given by:

$$V_c = V_{inv} = \frac{1}{(1-D_{av})} V_{DC} \quad \dots (3)$$

Where, V_{DC} is the input DC voltage. Substituting the equation (2) in (3) gives the inverter voltage V_{inv} using the SPWM and the THPWM schemes, and they are given in (4). From (4), the output fundamental peak phase voltage $V_{\phi 1}$ will be as given by (5) for the SPWM and the THPWM schemes.

$$V_{inv} = \frac{4\pi}{(2\pi - 3\sqrt{3}M)} V_{DC} \quad \text{SPWM}$$

$$V_{inv} = \frac{2\pi}{(\pi - 3M)} V_{DC} \quad \text{THPWM} \dots (4)$$

$$V_{\phi 1} = \frac{2\pi M}{(2\pi - 3\sqrt{3}M)} V_{DC} \quad \text{SPWM}$$

$$V_{\phi 1} = \frac{2\pi M}{(\sqrt{3}\pi - 3\sqrt{3}M)} V_{DC} \quad \text{THPWM} \dots (5)$$

The inductor current ripples can be calculated by (6) assuming low variations of capacitor voltage, where the desired capacitance can be obtained from (7).

$$L \approx \frac{KMVin v}{6\pi f_1 \Delta I_L} + \frac{D_{max} V_{Dc}}{2fs \Delta I_L} \quad \dots (6) \quad C \approx$$

$$\frac{KMIDc}{6\pi f_1 \Delta V_{inv}} + \frac{(1-D_{min})IDc}{2fs \Delta V_{inv}} \quad \dots (7)$$

Where, IDC and $I\phi_1$ are the average input DC current and the peak value of the fundamental output phase current respectively, ΔI_L is the overall inductor current ripple including the low frequency component, ΔV_C is the overall capacitor voltage ripple including the low frequency component, and K is a constant given by:

$$K = \begin{cases} \frac{3\sqrt{3}}{8\pi} & \text{SPWM} \\ \frac{27-4\pi\sqrt{3}}{36\pi} + \frac{3}{35\pi} & \text{THPWM} \dots (8) \end{cases}$$

And D_{min} , and D_{max} are the minimum and the maximum values of the duty cycle can be calculated by (9), and (10):

$$D_{min} = \begin{cases} \frac{1}{2} + \frac{1}{4}M & \text{SPWM} \\ \frac{1}{2} + \frac{2\sqrt{3}}{9}M & \text{THPWM} \dots (9) \end{cases}$$

$$D_{max} = \frac{1}{2} + \frac{1}{2}M \quad \text{SPWM, THPWM} \dots (9)$$

3. SIMULINK MODEL AND SIMULATION RESULTS

3.1 Simulink Parameters

A MATLAB/SIMULINK model has been build considering the parameters given in TABLE 1 using SPWM and THPWM modulations.

Table 1: Simulink parameters of the 2.0 KW Split-Source Inverter (SSI).

Graphics	Equation used	SPWM	THPWM
Required M	(5)	0.8704	0.7536
V_{inv}	(4)	713	713
D_{min}	(1), (2)	0.7175	0.79
D_{max}	(1), (2)	0.9351	0.8768
Required L(mH)	(6)	9.5	2.7
Required C(μ f)	(7)	620	180

4. SIMULINK MODEL

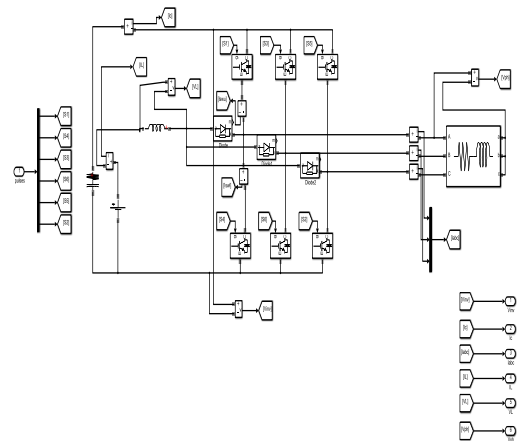


Fig.4: Simulink model of SSI.

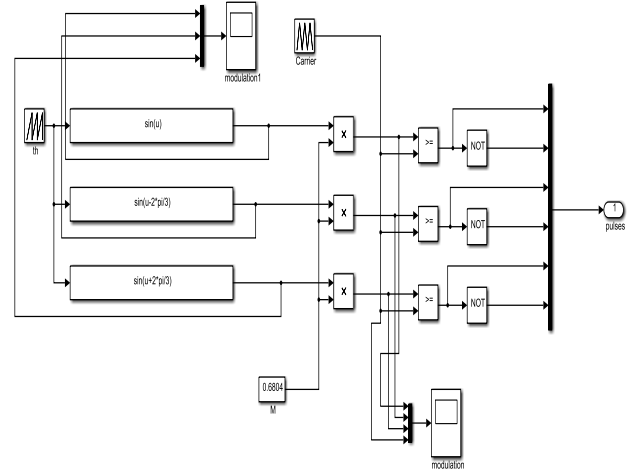


Fig.5: Subsystem SPWM.

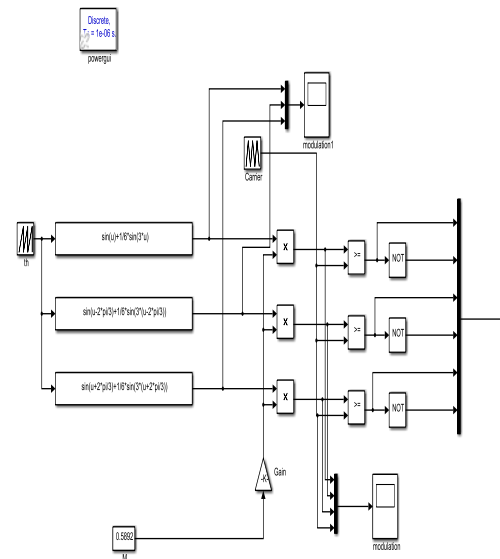


Fig.6: Subsystem THPWM

Fig.4 shows the SIMULINK model of the split-source inverter (SSI) using the parameters given in TABLE 1. Fig. 5 & 6 shows the subsystems to generate the gate pulses for the switches in SPWM and THPWM modulation schemes.

4.1 Simulation Results

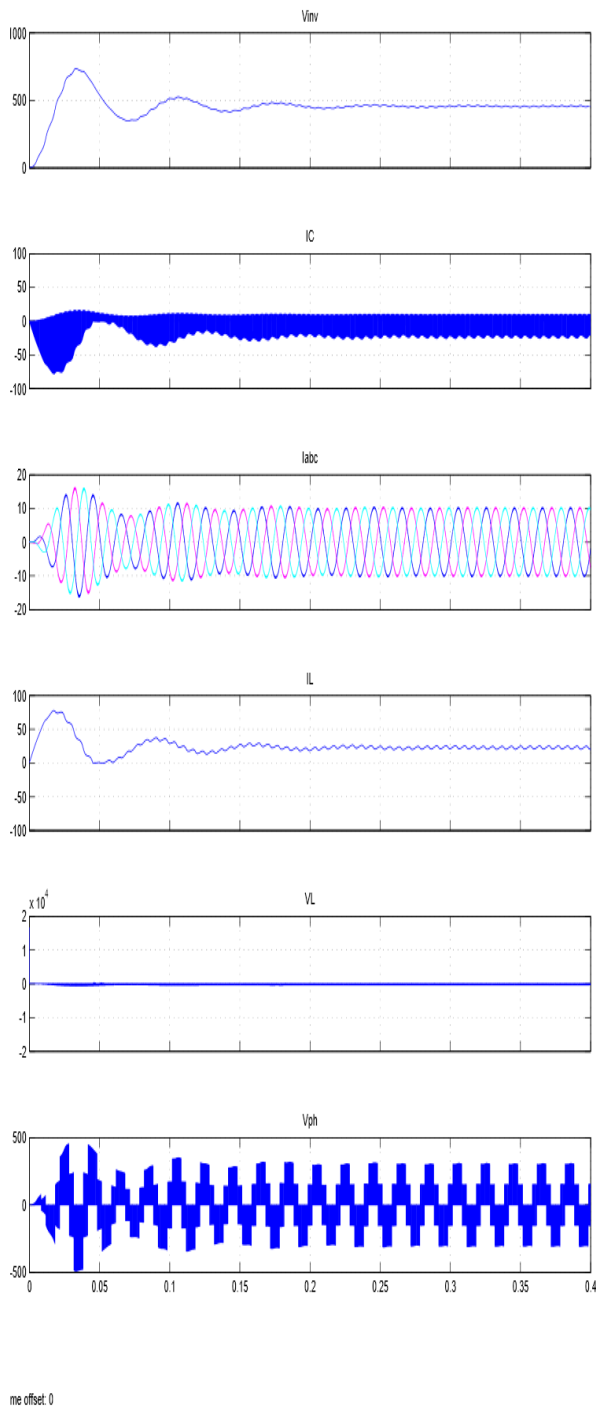


Fig.7: Simulation results using the SPWM.

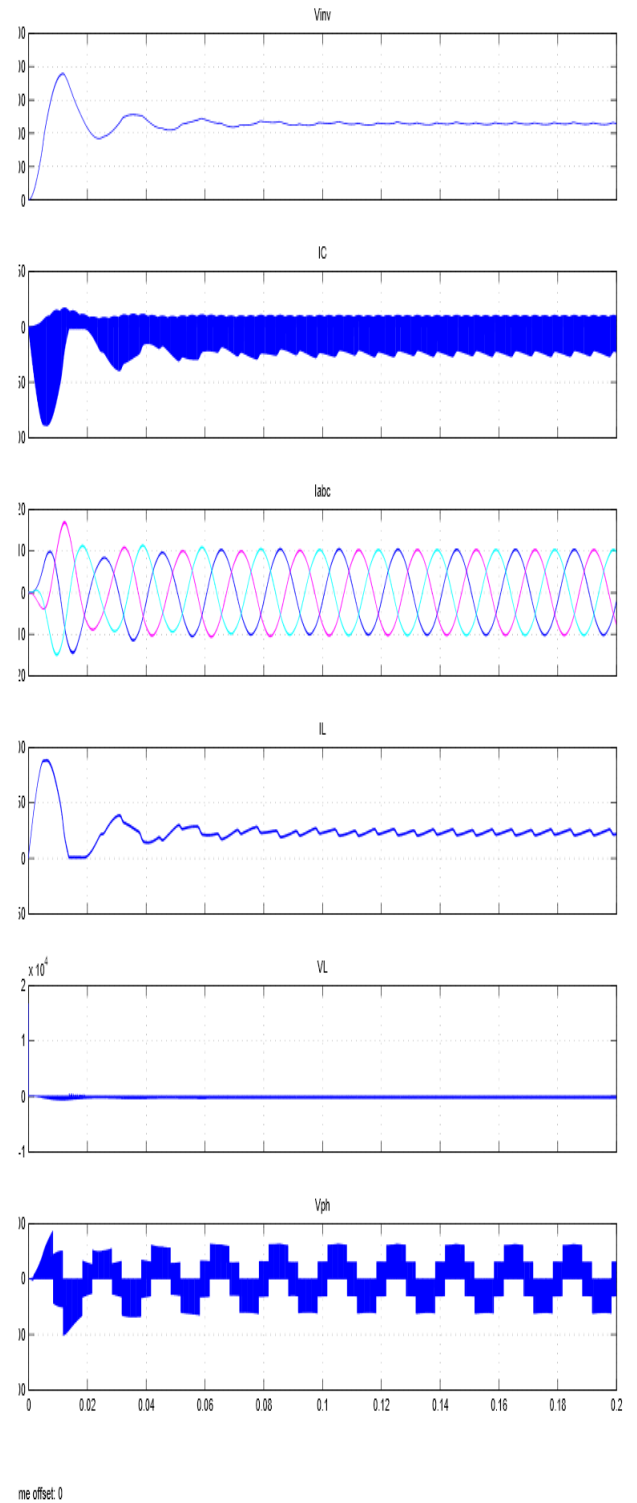


Fig.8: Simulation results using the THPWM.

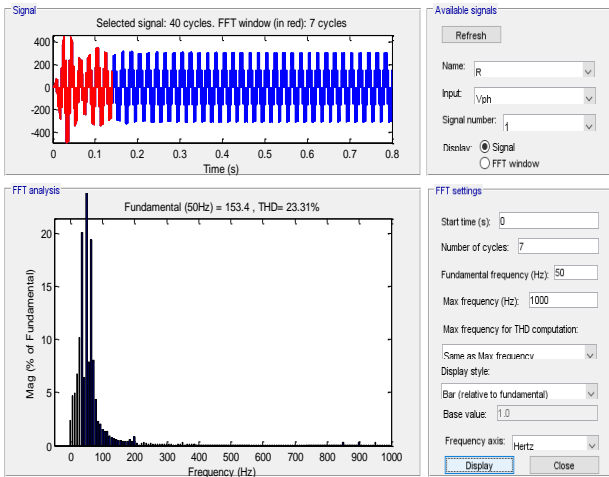


Fig.9: FFT Analysis of output phase voltage in SPWM modulation.

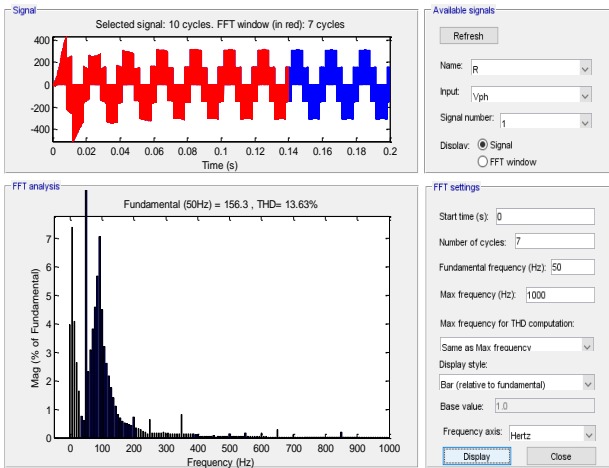


Fig.10: FFT Analysis of output phase voltage in THPWM modulation.

Fig.7& 8 shows the simulation results using both modulations. From this we can see that the V_{inv} is not constant but in the case of THPWM its ripple is less compared to SPWM. From the FFT analysis of output phase voltage shown in Fig.9& 10 we can see that in the case of SPWM modulation THD is 23.3% and in case of THPWM modulation its 13.63% only.

5. CONCLUSION

In this paper two modulation schemes have been examined for the three-phase SSI and the results obtained showed that it is better to use the THPWM instead of the SPWM, for less passive components requirements. On the other hand, in the case of SPWM modulation THD is 23.3% and in case of THPWM modulation its 13.63% only. In future another modulation scheme can be examined in order to eliminate the low-frequency component in the inductor current and the capacitor voltage.

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