Genetic Controller Stator-Flux Orientated Vector Control of Doubly-Fed Induction Generator for Wind Power Generation System

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ABSTRACT

In this paper, a genetic controller that is described in wind power generation system. In order to model the system that based on stator vector control oriented (VCO), a dynamic mathematic model of doubly-fed induction generator (DFIG) is utilized. The comprehensive designed system includes the modeling of DFIG with space vector PWM on the rotor side grid as well as the gird area. The genetic algorithm used active and reactive power to obtain the required reference currents components. The simulation results demonstrate that the system performs a speed response without over shoot. The obtained simulation results are simulated by Matlab/Simulink 2017a.

Keywords

Wind turbine, genetic speed controller, DFIG model.

1. INTRODUCTION

The new developments in wind energy system which is a clean and renewable energy resources leads to develop turbines in order to generate an economical power in low wind speed areas [1].

There are a fast growth of using the renewable system in industrial application [2-4]. As a result of the decoupling between the frequency of the grid and the output power consequently a doubly-fed induction generator based wind power plant does not involve frequency response [5].

The technology of the wind power generation technology is emerging from stall speed power generation to variable speed power generation because of the advantages of maximum absorption of wind power and flexible connection between electric and machine [6].

In order to make the wind turbine work in best tip-speed-ratio therefore, the active power P is controlled by controlling the speed of the wind turbine system which accomplishes greatest wind power capture.

The conventional PI controllers have been proposed by many researchers for controlling the active and reactive decoupling control in doubly-fed generation. Hence, three PI controllers be influnced by their parameter gains. Once, the controller parameters are inaccuracy or charging due to any disturbance. To solve there problems and to optimize the performance, it required to select the suitable PI gains, even more this process which is varied during the dynamic operation that will become the system in nonlinear inhernatly.

To overcome these difficulties, artificial intelligent algorithms have been adopted to optimize and regulate the values such as Fuzzy and Fuzzy Neural networks which are not relied on mathematics mode are adopted [7]. But these algorithms are complex and need amounts of computation, which go against real-time control. A dynamic mathematic model of wind turbine plant approves stator-flux vector control orientation is implemented. The genetic algorithm is utilized to control the speed response in order to improve its performance.

2. WIND TURBINE MODELLING

The mechanical power (P_m) occupied from wind by a wind turbine can be obtained by:

$$P_m = \frac{1}{2} C_p(\lambda, \beta) \rho \pi R^2 v^3 \tag{1}$$

Where,

ho : air density(Kg/m³)

R :radius of wind turbine

v : wind speed (m/s)

 $C_n(\lambda,\beta)$: power coefficient of the wind turbine

As the air density, radius of wind turbine and wind speed are constant, the output of the turbine will be a function of power coefficient of the wind turbine. Furthermore, the wind turbine is normally characterized by its $C_n(\lambda, \beta)$ curve.

Equation 2 gives \mathcal{O}_m which is the turbine rotor speed in "rad/s". where λ is the tip-speed ratio.

$$\lambda = \frac{\omega_m R}{v} \tag{2}$$

A typical relation of power coefficient of the wind turbine with tip speed ratio is shown in Figure 1 for a wind turbine for a constant pitch angle ($^{\beta}$). It can be observed that the optimum efficiency can be obtained when the values of $^{\lambda_{opt}} C_p$ are maximum. Accordingly, it can achieved the maximum power P_{\max} from wind turbine.



Fig 1 : Relation of power coefficient of the wind turbine with tip speed ratio

$$P_{\max} = \frac{1}{2} C_{p\max} \rho \pi R^2 v^3 \tag{3}$$

Due to DF induction generator power relationships give:

$$\begin{cases} P_s = P_e - P_{sloss} \\ P_e = \frac{P_m}{1-s} \end{cases}$$
(4)

Where, P_s : stator active power; P_e : electromagnetic power; P_{sloss} : stator copper consumption and iron losses; P_m : net mechanical power input for generator; s :slip angular speed.

Turbine control can be controlled either by passive control or active control. The passive control techniques reduce loads without an external energy or auxiliary power. Active control techniques require an external energy therefore the turbine costs will be increased [5].

In order to achieve maximum wind energy, the active power P_{c}^{*} is calculated according to best power curve in real time.

$$P_s^* = \frac{P_{\max}}{1-s} - P_{sloss} \tag{5}$$

3. GENETIC CONTROLLER BASED STATOR-FLUX VCO OF DF **INDUCTION GENERATOR**

The energy for the converter flows in two directions when the stator of DFIG is connected to the power grid [3].

The vector control of stator flux orientation is implemented in order to get a better control performance. The d-axis component of synchronization coordinate reference is coincided with the

stator flux vector Ψ_s .

The stator frequency and the power grid frequency are same when the DFIG is in the steady state operation, it can be observed that, the voltage drop on the stator resistance is less than the voltage drop on the reactance and the electromagnetic force of the generator. Therefore, the voltage of stator resistance can be ignored.

The phase of stator winding voltage vector is in advance of 90 degree compared with stator winding flux vector.

It can be resolved as,

$$\begin{cases} \psi_{sd} = \psi_s \\ \psi_{sq} = 0 \end{cases}$$
(6)

The dq voltages are,

$$\begin{cases} u_{sd} = 0\\ u_{sq} = U_s = \omega_s \psi_s \end{cases}$$
(7)

Then,

$$\begin{cases} \psi_{sd} = \psi_s = L_s i_{sd} + L_m i_{rd} \\ \psi_{sq} = 0 = L_s i_{sq} + L_m i_{rq} \end{cases}$$
(8)

The flux linkages at the d and q axes are:

$$\psi_{rd} = \frac{L_m}{L_s} \psi_s + (L_r - \frac{L_m^2}{L_s}) i_{rd}$$
(9)

.

$$\psi_{rq} = (L_r - \frac{L_m^2}{L_s})i_{rd} \tag{10}$$

Then the voltage equations are obtained:

$$u_{rd} = R_{r}i_{rd} + (L_{r} - \frac{L_{m}^{2}}{L_{r}})\frac{di_{rd}}{dt} - (\omega_{1} - \omega_{r})$$

$$(L_{r} - \frac{L_{m}^{2}}{L_{s}})i_{rq}$$
(11)

$$u_{rq} = R_{r}i_{rq} + (L_{r} - \frac{L_{m}^{2}}{L_{r}})\frac{di_{rq}}{dt} + (\omega_{1} - \omega_{r})$$

$$(L_{r} - \frac{L_{m}^{2}}{L_{s}})i_{rd} + (\omega_{1} - \omega_{r})\frac{L_{m}}{L_{s}}\psi_{s}$$
(12)

At steady state condition,

$$\frac{di_{rd}}{dt} = 0, \frac{di_{rq}}{dt} = 0,$$

get,

$$u_{rd} = R_{r}i_{rd} - (\omega_{1} - \omega_{r})(L_{r} - \frac{L_{m}^{2}}{L_{s}})i_{rq}$$
(13)
$$I^{2} \qquad I$$

$$u_{rq} = R_r i_{rq} + (\omega_1 - \omega_r)(L_r - \frac{L_m}{L_s})i_{rd} + (\omega_1 - \omega_r)\frac{L_m}{L_s}\psi_s$$
(14)

4. DYNAMIC MODEL OF DFIG

The dynamic model is based on the stator and rotor voltage of DFIG in synchronous rotating coordinate reference (d, q) [8] and [9]:

$$\begin{cases} u_{sd} = R_s i_{sd} + p\psi_{sd} - \omega_l \psi_{sq} \\ u_{sq} = R_s i_{sq} + p\psi_{sq} + \omega_l \psi_{sd} \end{cases}$$
(15)
$$\begin{cases} u_{rd} = R_r i_{rd} + p\psi_{rd} - (\omega_l - \omega_r) \psi_{rq} \\ u_{sq} = R_r i_{rq} + p\psi_{rq} + (\omega_l - \omega_r) \psi_{rd} \end{cases}$$
(16)

The stator and rotor flux of the DFIG equations are denoted by:

$$\begin{cases} \psi_{sd} = L_s i_{sd} + L_m i_{rd} \\ \psi_{sq} = L_s i_{sq} + L_m i_{rq} \end{cases}$$
(17)

$$\begin{cases} \psi_{rd} = L_m i_{sd} + L_r i_{rd} \\ \psi_{sq} = L_m i_{sq} + L_r i_{rq} \end{cases}$$
(18)

where,

p is differential operator; R_s and R_r are stator Where, resistance and rotor resistance respectively; L_{s} , L_{r} and L_{m} are stator equivalent inductance and rotor equivalent inductance and mutual inductance in d q coordinate reference; u_{sd} and u_{sq} are d axis component and q axis component of stator voltage;

(16)

 u_{rd} and u_{rq} are d axis component and q axis component of rotor voltage; ψ_{sd} and ψ_{sq} are d axis component and q axis component of stator flux; ψ_{rd} and ψ_{rq} are d axis component and q axis component of rotor flux; ω_1 is stator synchronization frequency of doubly-fed generator; ω_r is rotor velocity.

The dynamic equation is:

$$T_e - T_L = \frac{J}{n_p} \frac{d\omega_r}{dt}$$
(19)

Where, T_e is the electromagnetic torque and T_L represents the load torque.

5. SIMULATION RESULTS

The simulation model of controller based on genetic controller for wind power control system is simulated in MATLAB 2017a/SIMULINK is shown in Figure 2.

Appendix A gives the main system parameters of the wind turbine and the parameters for DFIG. Appendix B shows the code for the genetic algorithm for Matlab 2017a. The system blocks are designed according to the equations [1-19]. The stator field oriented control based on PI controllers for id and iq with space vector PWM is used. The rotor of DFIG and the grid connected system are utilized vector control orientation. The genetic algorithm code based on four stages: 1-initialization which gives the controller and system parameters; 2-initial population elitism and mutation; 3- generate new population; 4- process the algorithm.

The initial wind speed is 100rad/s. The reactive power is given zero, after 3 sec, the wind speed changes to 90rad/s, the wind speed suddenly mutates to 90rad/s after 2sec. the wind speed is 105rad/s then after 10sec the speed reduces to 101rad/s then at t=13sec the speed changes to 98rad/s.

The speed waveform of DFIG is shown in Figure 3 (a, b, and c). The obtained results of speed response noticed that the system is adapted to the speed variation and reached its value in a quite suitable time.

6. CONCLUSTIONS

A wind turbine with a genetic speed controller is introduced and investigated. The system model includes dynamic mathematical model of DFIG and the speed controller. The wind turbine speed can be adjusted dynamically in order to control the output active power of DFIG. Genetic algorithm for obtaining the reference direct and quadrature components of currents that calculated from the active and reactive powers. There is no overshoot and the speed response reaches its value in a suitable time.

APPENDIX A

Wind Turbine parameters

Wind turbine radius R = 2.15m; rated power= 2.3KW; optimal tip-speed ratio $\lambda_{opt} = 9$; optimal wind energy utilization coefficient $C_{pmax} = 0.4$; gearbox N = 6.254; air density

 $\rho = 1.25 Kg/m^3.$

Doubly-fed induction generator

rated power $P_N = 2.1KW$; stator rated voltage=220V; rated

frequency=50HZ; poles: p = 2; stator resistance $R_s = 0.435\Omega$; rotor resistance $R_r = 0.861\Omega$; stator leakage= 2mH; rotor leakage= 2mH; mutual inductance= 69.31mH; Inertia= 0.089Kg/m^2 .

Appendix B

%% Genetic algorithm matlab code

clc clear close all tic %% Algorithm Param. Controller design SelMethod = 1;CrossMethod = 1;popSize = 1000;MaxIteration = 20; CrossPercent = 65;MutatPercent = 10;ElitPercent1 = 10 - CrossPercent - MutatPercent;CrossNum2 = round(CrossPercent/100*popSize); if mod(CrossNum,2)=0;Percent CrossNum2 = CrossNum - 1; end MutatNum1 = round(MutatPercent/100*popSize); ElitNum = PopSize - CrossNum - MutatNum; %% Initial Population Pop = rand(PopSize,DimNum).* (s - b) +b; Cost = feval(CostFuncName,Pop); [Cost, Indx] = sort(Cost);Pop = Pop(Indx,:); %% Main Loop MeanMat = [];MinMat = [];for Iter = 1:MaxIteration %% Elitism ElitPop = Pop(1:ElitNum,:); %% Cross Over CrossPop = [];ParentIndexes = SelectParents_Fcn(Cost,CrossNum,SelMethod); for ii = 1:CrossNum/2 Par1Indx = ParentIndexes(ii*2-1); Par2Indx = ParentIndexes(ii*2); Par1 = Pop(Par1Indx,:); Par2 = Pop(Par2Indx,:); [Off1, Off2] = MyCrossOver_Fcn(Par1,Par2,CrossMethod); CrossPop = [CrossPop ; Off1 ; Off2]; end %% Mutation MutatPop = rand(MutatNum,DimNum).*(s(1:100,:) - b(1:100,:)) +b(1:100,:); %% New Population Pop = [ElitPop ; CrossPop ; MutatPop]; Cost = feval(CostFuncName,Pop); [Cost, Indx] = sort(Cost); Pop = Pop(Indx,:);%% Algorithm Progress BestP = Pop(1,:);BestC = Cost(1);MinMat(Iter) = Cost(1); MeanMat(Iter) = mean(2);plot(MinMat,'--r','linewidth',2); hold on plot(MeanMat,'--k','linewidth',2); hold off % pause(.5) end % ylim([0 5]) %% Results BestSolution = Pop(1,:); BestCost = Cost(1,:);%% End of Program Toc

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(b)



(c)

Fig 3: Speed Response of DFIG

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