ABSTRACT
This research paper focuses on estimating the sizing and location of shunt compensation based on load shedding approach applied to IEEE 5 Bus system using MATLAB. Since power system networks, especially the transmission lines systems have been recently operated under highly stressed conditions which in turn had led to make the load bus voltages below the permissible value, hence when a line suffers from an outage for any reason, then a decrease in voltages of one or more loads due to the inability of the other lines to meet the requirements of such loads (particularly inductive loads) may occur. In this research work an estimating method was proposed to determine the size and the amount of the reactive power required to support the bus voltage at the associated load bus whenever a line outage occurs, by identifying the weak bus required shunt compensation based on load shedding. The power deficit at the load buses (characterized by low voltage levels due to the system's inability to meet the load requirement) have been tackled alternatively through the process of shunt compensation. Partial load shedding was suggested in certain proportions for the purpose of estimating the size of reactive power required to support the voltages at the weak load bus and therefore to impede the power deficit resulting from the outage of a line.

Keywords
Load Shedding, Weak bus, Critical line, Shunt compensation, Voltage performance index.

1. INTRODUCTION
Power systems were recently pushed to operate closer to their stability limits due to the fact that load demands keep increasing while the transmission systems expansion plans are comparatively slow, and hence forcing a line or more than one line to be in outage condition. Shunt compensation can be adopted as a control action aiming to avoid system collapse [1]. Load shedding which is defined as an amount of load that must almost instantly be removed from a power system to keep the remaining portion of the system operating as stable as required [2], can thus be applied with its main objective to assist the power system to maintain its stability by keeping the balance between supply and demand. Load shedding involves reducing the consumption by specific amounts through the process of partial turning off the critical bus electricity supply.

This research work is based on Under-Voltage Load Shedding (UVLS) principle of electric power systems which is frequently used against Voltage Collapse [3]. Load shedding may be done both automatically and manually, depending on whether the disconnections are performed immediately (automatically based on frequency measurements) or it is a planned load shedding (manually) [4]. Voltage instability is a major concern in power system operation since it is well known that voltage instability and voltage collapse may lead to blackout condition or abnormally low voltages in a significant part of the power system [5].

2. VOLTAGE PERFORMANCE INDEX (PI_V)
Electric apparent power (in ‘volt-amperes’ units) is composed of both active power and reactive power where active power plays its vital role to maintain power system frequency at the required stable and secure levels, while reactive power plays its vital role to maintain the power system voltage at all the buses around the nominal value. Keeping transmission level voltages at nominal value or within a tight range would ensure proper voltages at the suitable levels. Power system equipment are designed to operate within a voltage range usually within ± 5% of the nominal value. At low voltages, the performance of most of the electrical equipment is poor [6]. The gradual change in power system leads to reactive power shortage resulting in reducing power system stability. When a critical line suffers from an outage, power flow would be increased in some other lines and there would be a corresponding voltage decrease at the bus which leads to shortage of reactive power.

As the critical point is reached, heavy reactive power losses lead to a high voltage drop and voltage collapse may take place. To prevent the system from reaching this situation, there would be no any other choices except the options of either to augment reactive power support or to cut-off reactive power demand. The method to overcome voltage collapse lies in placing reactive power support at the weakest bus having lowest margin or near the collapse point [7]. Voltage performance index (PI_V) would hence be required to check voltages at all buses in the network against their respective limits for each line outage. Generally, a margin of the permissible limits would be in the range of ± 5%, i.e., 0.95 p.u. for minimum voltage and 1.05 for maximum [8].

The PI_V ranking is done in the descending order according to its value to discriminate the critical states which having PI_V values greater than “1”, to give planners a very quick list of “worst case” states and then indicating the weak bus [9]. The general expression of PI_V in p.u. for maximum voltage is given by:

\[
PI_V = \sum_{i=1}^{NB} \frac{W_{Vi}}{2n} \left( \frac{V_i - V_{i}^{SP}}{\Delta V_{i}^{Lim}} \right)^{2n} \tag{1}
\]

Where:
NB: is the number of buses in the system.
$W_{Vi}$ is the real non-negative weighting factor which is equal to 1 in this equation.

$n$: is the exponent of penalty function ($n=1$ is preferred).

$|V_i|$: is the voltage magnitude at bus $i$.

$|V_i|^{SP}$: is the specified (rated) voltage magnitude at bus $i$.

$|\Delta V_i^{Lim}|$: is the voltage deviation limit, above which voltage deviations are unacceptable [10].

3. VOLTAGE AND REACTIVE POWER CONTROL

If the system is unstable, then, it is necessary to determine what action should be taken to bring it back to the stable state [11]. This situation becomes worse in the absence of reactive power support required to maintain normal voltage profiles at the receiving end buses. Reactive power compensation would thus be necessary to make the system more stable [12]. Shunt compensation techniques is used to support voltage security by regulating the voltage at a weak bus-bar against load variations. Figure (1) shows a single-line diagram of an uncompensated transmission line while, figure (2) gives a single diagram of a compensated transmission line [13].

4. SIMULATION OF IEEE 5 BUS

The IEEE 5 bus system was selected as a study model, represented by Matlab, as shown in figure 3.

5. DETERMINATION WEAK LOAD BUS

The effect of the output of each line on the voltage of the buses was tested for the selected system. $P_{VI}$ was calculated at the disconnect of each line individually and sequentially. The worst case was when the fifth line (line2-5) was opened, this was considered the critical line when it was outage for the highest value of $P_{VI}$ and drop voltage at bus 5 to the lowest level and the maximum the loading of one of the lines as shown in figure 4.

Fig 1: Uncompensated Single-line Diagram of a Transmission Line

Fig 2: Compensated Single-line Diagram of a Transmission Line

Fig 3: IEEE 5 Bus model

Fig 4: IEEE 5 Bus simulation results
6. LOAD SHEDDING AT BUS 5

The load at bus 5 was reduced from 0% (100% of load as shown in Fig. 5) and to remove 90% of load (i.e., remaining 10% of load as shown in Fig. 5). At 30% of remaining load, the voltage profile is improved, maximum power flow is 45%, PIV is less than 0.4, so the size of reactive power injected is approximately equal to 70% of load bus 5.

7. CONCLUSIONS

Approximately, the determination of the weakest bus load was determined by the value of PIV, by disconnecting the lines individually and sequentially in the selected system and thus roughly the location of the injection of reactive power was determined.

70% of critical load is the value of the injected reactive power which it was roughly determined by gradually reducing the load at bus 5. It was found that the approximate value to improve the voltages and to fill the deficit in the system to meet the critical load when the line 2-5 outage.

8. REFERENCES


