

Frequency Response Analysis for T-S Fuzzy Systems

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ABSTRACT

Frequency response is an important physical quantity in audio systems for minimizing audible distortion and in control systems for assessing system relative stability. For linear time-invariant systems (LTI systems), frequency response has one-to-one relationship to system impulse response. However, the LTI systems-based analysis cannot describe nonlinear frequency response well. T-S fuzzy systems are based on fuzzily blending several linear subsystems and are widely used to describe nonlinear systems behavior in various fields. Recently, researcher tried to obtain frequency response of T-S fuzzy systems through the assumption that the same fuzzy relationship exists in both time domain and frequency domain. In this paper, we focus on deriving fuzzy frequency response from both *basic* definitions of frequency response and previously proposed neural-network-based fuzzy blending feature to find out the limitations, the range of frequency response for T-S fuzzy systems. Steady-state system response is additionally discussed and tested with two active magnetic bearing systems.

Keywords

Fuzzy systems, frequency response, relative stability

1. INTRODUCTION

Fuzzy logic (an extension of multivalued logic) is always used to describe the classes of objects or data which are vague and lack certainty. Recently, T-S type fuzzy systems were widely used to describe the dynamic behavior of various *physical systems* and have demonstrated to be universal approximations of any smooth nonlinear systems [1-3]. Various fuzzy controllers for physical systems have been developed since 2000. In 2016 Wiktorowicz further used frequency domain methods to design output-feedback-based adaptive fuzzy controllers [4]. Kluska and Zabinski recently proposed PID-like adaptive fuzzy controllers [5]. Zhao and coworkers developed observer-based H_∞ controllers for spacing type-II T-S fuzzy systems [6]. We demonstrated that affine T-S fuzzy systems possess more advantages than T-S fuzzy systems in nonlinear modelling [7]. Wang and Yang introduced dilated linear matrix inequality to develop piecewise controllers for affine T-S fuzzy systems [8, 9], and proposed piecewise-Lyapunov-functions-based H_∞ controllers for affine T-S fuzzy systems in finite frequency domain [10]. Qiu and coworkers used quantized measurements to develop observer-based piecewise output-feedback controllers for affine T-S fuzzy systems [11]. Recently, research focus on the development of filter design of T-S fuzzy models of physical systems. Liu and Yang discussed sensor fault detection for systems in finite domain [12]. Hellani and coworkers developed finite-frequency-based H_∞ filter design [13]. Li and coworkers proposed finite-frequency-based $L_2 - L_\infty$ filters [14].

Fuzzy set theory shows great potential in dealing with

biological data and modelling *biological systems* because of the use of linguistic variables and fuzzy relationship. Luo and An took a review of fuzzy set theory in device control, biological control, classification and pattern recognition, and prediction and association [15]. Komiyama and coworkers emphasized that fuzzy interactions always exist in cell macromolecular nanoarchitectonics [16]. Abyad and coworkers used T-S fuzzy models to describe biomass growth processes and then optimal fuzzy control was used to control the process [17]. Bordon et al. used fuzzy logic to achieve the quantitatively modelling of repressilators with unknown kinetic data [18]. Liu and coworkers introduced fuzzy Petri nets for biological system modelling and discussed the capacities and applications [19]. They further proposed a hybrid of continuous Petri nets and fuzzy inference systems to achieve integrated modelling of biological systems with uncertainties [20]. Zhu and coworkers used fuzzy neural networks as inverse systems to achieve decoupling control of marine biological enzyme fermentation processes [21]. An adaptive T-S type neural-fuzzy scheme was proposed to achieve the fuzzy modeling of multi-inputs multi-outputs *biological systems* (small-scale genetic networks, branch pathways and cascade networks systems) [22]. The number of generated rules depends on the number of input variables of underlying systems and the division of the input space: There are 3^n rule numbers for an n -dimensional biological system with each input variable being divided into three intervals. To reduce the number of rules, researchers tried to construct biological fuzzy systems with a fixed number of rules. However, to determine the number of rules which are sufficient to ensure the accuracy researchers should fully understand underlying biological systems. This will lose the essence of adaptive T-S type neural-fuzzy modeling.

Frequency response is one of important analysis methods in audio, control and statistic fields. For linear time-invariant system, sinusoidal input signals generate sinusoidal output signals with different amplitudes and phases determined by system frequency response. However, such good characteristics do not exist in nonlinear systems. T-S fuzzy systems, at a time instant, are the fuzzy blending of their linear subsystems. This feature prompted researchers to explore the feasibility of frequency analysis of T-S fuzzy systems. Kumar and coworkers proposed a probabilistic data-driven geospatial fuzzy frequency ratio for avalanche susceptibility mapping [23]. Ali and coworkers used frequency domain analysis (power spectral density graphs) to get both primary and average frequencies as fuzzy inputs for rotating machinery vibration analysis [24]. Ferreira and Serra tried to propose a definition on fuzzy frequency response [25]. They used the proposed estimation methods of frequency response to deal with experimental data of mechanical structures of aircraft and aerospace vehicles [26], and data from flexible robot arms [27]. They also do a case study for pH neutralization process [28]. However, an important issue was ignored that membership functions of fuzzy systems are

time-varying functions, and the corresponding normalized firing strength cannot be represented by fixed functions. In this study, we shall stem on the principle of frequency response to define the frequency response of T-S fuzzy systems.

2. FUZZY-NEURAL-NETWORKS-BASED FREQUENCY RESPONSE

Frequency response methods serves as the backbone of the classical control methods and still give shed light to such an important characteristic as robustness for modern control techniques. Musical notes generated by a guitar are related to its frequency response [29]. For linearly time-invariant systems, system outputs $y(t)$ are the convolution of system impulse response $h(t)$ and system inputs $u(t)$; $y(t) = h(t) * u(t)$, where the notation $*$ denotes the convolution operation. We then have $Y(j\omega) = H(j\omega)U(j\omega)$, where $Y(j\omega)$, $H(j\omega)$ and $U(j\omega)$ are, respectively, the Fourier transforms of $y(t)$, $h(t)$ and $u(t)$, and $H(j\omega)$ denotes system frequency response. However, there does not exist such a relationship in nonlinear systems although system inputs and outputs also have their corresponding Fourier transforms.

We have previously developed neural-fuzzy inference networks to capture the dynamic behavior of current/voltage-controlled 1/4-vehicle MagLev systems [7], car model systems [30], radial active magnetic bearing systems [31], half-car active suspension systems [32]. In this study, we shall derive the frequency response of T-S fuzzy systems based on previously proposed self-constructing neural-fuzzy inference networks in Fig. 1 which were used to realize T-S fuzzy modelling of various physical systems [7, 30-32].

The neural-fuzzy inference network in Fig. 1 possesses six layers [7]. Layers 1 and 6 are the input layer and output layer, respectively. There are four hidden layers which are corresponding to fuzzification, fuzzy blending, normalization and defuzzification of fuzzy logic inference systems. Each node has finite weighted fan-in connections to the last-layer nodes and fan-out connections to the next-layer nodes.

Layer 1: The nodes denote input variables and directly transmit input variables to the next layer.

Layer 2: This layer performs fuzzification and each node in this layer denotes a linguistic label. In this study, we choose Gaussian distributions as membership functions to achieve smooth and general fuzzification.

Layer 3: This layer performs fuzzily blending operation. Each node describes one fuzzy logic rule.

Layer 4: This layer performs normalization to let the summation of firing strength of rules be one.

Layer 5: This layer is the consequence layer which performs Sugeno-type defuzzification.

Layer 6: This layer performs defuzzification operations and each node corresponds to one output variable of underlying systems.

The numeric input variable x_i is directly transmitted into the network in Layer 1, and then fuzzified to fuzzy term sets T_{ij} which possess Gaussian membership functions with mean m_{ij} and standard deviation σ_{ij} in Layer 2. The firing strength of each fuzzy rule are obtained in Layer 3 and the corresponding normalized firing strength are then estimated in Layer 4. The linear-system-type rule consequences are generated in Layer 5 and system outputs are obtained through Sugeno-type defuzzification in Layer 6.

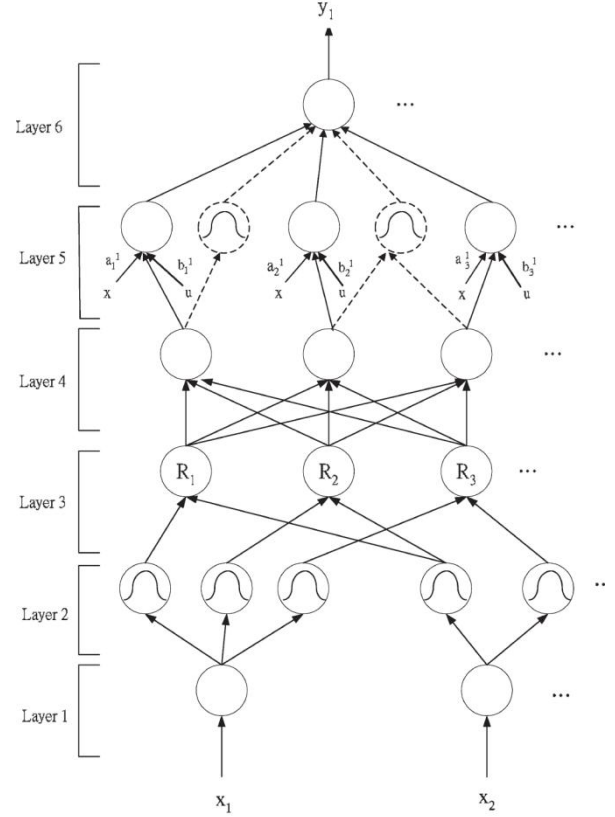


Fig. 1: Neural-fuzzy inference network for T-S fuzzy systems [7].

According to fuzzy set theory and the scheme of neural fuzzy inference systems in Fig. 1 [7], we know at any time instance the overall dynamic behavior of T-S fuzzy systems can be described as fuzzily blending the dynamic behavior of their linear subsystems. Therefore, the unit impulse response of the entire fuzzy system is $h(t) = \sum_i^n \mu_i(x(t))h_i(t)$, where $h_i(t)$, $\mu_i(x(t))$ are the unit impulse response of the i -th subsystem and the corresponding firing strength, respectively. Then, the following theorems are derived.

Theorem 1: The frequency response of the entire fuzzy system is

$$H(j\omega) = \sum_i^n M_i(x(j\omega)) * H_i(j\omega), \quad (1)$$

where $*$ denotes the convolution operator; $H_i(j\omega)$ and $M_i(x(j\omega))$ are, respectively, the corresponding Fourier transform of the unit impulse response $h_i(t)$ and the normalized firing strength $\mu_i(x(t))$, i.e., $H_i(j\omega) = \mathcal{F}\{h_i(x(t))\}$ and $M_i(x(j\omega)) = \mathcal{F}\{\mu_i(x(t))\}$.

Proof: At any time-instant, the unit impulse response of the entire fuzzy system is $h(t) = \sum_i^n \mu_i(x(t))h_i(t)$. The system frequency response is then obtained through Fourier transform,

$$\begin{aligned} H(j\omega) &= \mathcal{F}\{h(t)\} = \mathcal{F}\left\{\sum_i^n \mu_i(x(t))h_i(t)\right\} \\ &= \sum_i^n \mathcal{F}\{\mu_i(x(t)) * h_i(j\omega)\} \\ &= \sum_i^n M_i(x(j\omega)) * H_i(j\omega) \quad (2) \quad \blacksquare \end{aligned}$$

Therefore, the frequency response of the entire fuzzy

systems $H(j\omega) \neq \sum_{i=1}^n \mu_i(x(t))H_i(j\omega)$. Ferreira and Serra proposed a series of researches in fuzzy frequency response [25, 27, 33] which are all based on an assumption that the normalized firing strength $\mu_i(x(t))$ is a constant value μ_i and assume that $H(j\omega) = \sum_{i=1}^n \mu_i \cdot H_i(j\omega)$.

Theorem 2: In the frequency domain there does not exist a simple relationship between system outputs $Y(j\omega)$ and system inputs $U(j\omega)$:

$$Y(j\omega) \neq H(j\omega)U(j\omega), (3)$$

where $Y(j\omega)$ and $U(j\omega)$ are the Fourier transform of system output $y(t)$ and system input $u(t)$.

Proof: At any time-instant, system response is the fuzzily blending of all of subsystem response. We have

$$y(t) = \sum_{i=1}^n [\mu_i(x(t)) \cdot (h_i(t) * u(t))], (4)$$

where $*$ denotes convolution operators. We know Fourier transform is a linear operator. So, $Y(j\omega) = \mathcal{F}\{y(t)\}$ becomes

$$\begin{aligned} Y(j\omega) &= \sum_{i=1}^n \mathcal{F}\{\mu_i(x(t)) \cdot (h_i(t) * u(t))\} \\ &= \sum_{i=1}^n \mathcal{F}\{\mu_i(x(t))\} * (H_i(j\omega)U(j\omega)) \\ &= \sum_{i=1}^n M_i(x(j\omega)) * H_i(j\omega)U(j\omega) \\ &\neq H(j\omega)U(j\omega). \end{aligned} \quad (5) \quad \blacksquare$$

We know that the normalized firing strength $\mu_i(x(t))$ not only varies by time but also depends on subsystems. We cannot use a fixed function to describe the normalized firing strength even the Gaussian membership function is used. Therefore, there are no analytical solution for the corresponding Fourier transform, $M_i(x(j\omega))$. In the future we shall integrate block-based graphical methods and numerical methods to estimate $M_i(x(j\omega))$ and then to get a numerical approximation of $H(j\omega)$.

Theorem 3: $2\pi\delta(\omega) \min_i \inf_t h_i(t) \leq H(j\omega) \leq 2\pi\delta(\omega) \max_i \|h_i(t)\|_\infty$, where $\delta(\omega)$ is the impulse function.

Proof: $h(t) = \sum_{i=1}^n \mu_i(x(t))h_i(t)$. The corresponding Fourier transform is

$$H(j\omega) = \int_{-\infty}^{\infty} \sum_{i=1}^n \mu_i(x(t))h_i(t)e^{-j\omega t} dt. (6)$$

According to $\sum_{i=1}^n \mu_i(x(t)) = 1$, we obtain

$$\begin{aligned} \sum_{i=1}^n \mu_i(x(t))h_i(t) &\leq \sum_{i=1}^n \mu_i(x(t)) \cdot \sup_t h_i(t) \\ &= \sum_{i=1}^n \mu_i(x(t)) \cdot \|h_i(t)\|_\infty \\ &\leq \sum_{i=1}^n \mu_i(x(t)) \cdot \max_i \|h_i(t)\|_\infty \\ &= \max_i \|h_i(t)\|_\infty. \end{aligned} \quad (7)$$

$$\begin{aligned} \sum_{i=1}^n \mu_i(x(t))h_i(t) &\geq \sum_{i=1}^n \mu_i(x(t)) \cdot \inf_t h_i(t) \\ &\geq \sum_{i=1}^n \mu_i(x(t)) \cdot \min_i \inf_t h_i(t) \\ &= \min_i \inf_t h_i(t). \end{aligned} \quad (8)$$

Therefore, we have

$$\begin{aligned} \int_{-\infty}^{\infty} \min_i \inf_t h_i(t) e^{-j\omega t} dt &\leq H(j\omega) \\ &\leq \int_{-\infty}^{\infty} \max_i \|h_i(t)\|_\infty e^{-j\omega t} dt. \end{aligned} \quad (9)$$

We then obtain the following inequality because both $\max_i \|h_i(t)\|_\infty$ and $\min_i \inf_t h_i(t)$ are constants for the integral, and $\mathcal{F}\{e^{-j\omega_0 t}\} = 2\pi\delta(\omega - \omega_0)$.

$$2\pi\delta(\omega) \min_i \inf_t h_i(t) \leq H(j\omega) \leq 2\pi\delta(\omega) \max_i \|h_i(t)\|_\infty. \quad (10) \quad \blacksquare$$

3. STEADY-STATE SYSTEMS RESPONSE

Steward mentioned in [29] that frequency response is related to the steady state of a system when a harmonic function is applied as the input. In this section we demonstrate that the steady states response of T-S fuzzy systems are predictable when input signals are exponential functions, sine functions and cosine functions, even frequency response of underlying systems cannot obtain through analytical methods. However, there does not exist such a relationship that the responses to sine input signals and cosine input signals are exactly the real part and imaginary part of the response to exponential input signals, respectively.

Theorem 4: The steady state response $y_{ss}(t)$ of T-S fuzzy systems to harmonic input signals $u(t)$ is $y_{ss}(t) = u_0 \bar{H}(j\omega) e^{j\omega t}$ for $u(t) = u_0 e^{j\omega t}$, (11)

$$y_{ss}^s(t) = u_0 \bar{H}(j\omega) \sin(\omega t) \text{ for } u(t) = u_0 \sin(\omega t), (12)$$

$$y_{ss}^c(t) = u_0 \bar{H}(j\omega) \cos(\omega t) \text{ for } u(t) = u_0 \cos(\omega t), (13)$$

where $\bar{H}(j\omega) = \sum_{i=1}^n \mu_i(x_s) H_i(j\omega)$ and $\mu_i(x_s)$ is the normalized firing strength of the i -th subsystem at the steady state x_s . However, $y_{ss}^s(t) \neq I_m[y_{ss}(t)]$ and $y_{ss}^c(t) \neq R_e[y_{ss}(t)]$.

Proof: The steady state response is defined as $y_{ss}(t) \triangleq \lim_{t \rightarrow \infty} y(t)$ which is the fuzzily blending of the response of subsystems at the steady state, i.e., $y_{ss}(t) = \lim_{t \rightarrow \infty} \sum_{i=1}^n \mu_i(x(t)) [h_i(t) * u(t)] = \sum_{i=1}^n \mu_i(x_s) \lim_{t \rightarrow \infty} [h_i(t) * u(t)]$. For each subsystem which is linear time-invariant system, we have the following responses to harmonic inputs at the steady state,

$$\begin{aligned} h_i(t) * u(t) &= u_0 H_i(j\omega) e^{j\omega t}, \text{ for } u(t) = u_0 e^{j\omega t}, \\ &= u_0 H_i(j\omega) \sin(\omega t), \text{ for } u(t) = u_0 \sin(\omega t), \\ &= u_0 H_i(j\omega) \cos(\omega t), \text{ for } u(t) = u_0 \cos(\omega t). \end{aligned} \quad (14)$$

At the steady state x_s , the normalized firing strength $\mu_i(x_s)$ is a constant value. So, we obtain Eqs. (11)~(13) through setting $\bar{H}(j\omega) = \sum_{i=1}^n \mu_i(x_s) H_i(j\omega)$. $\blacksquare$

Theorem 4 is a prediction of the dynamic behavior of T-S fuzzy systems. The steady states of biological systems always depend on experimental environments. Therefore, we here use two physical systems to examine the prediction.

■ horizontal radial active magnetic bearings

We first consider an radial magnetic bearing system, as shown in Fig. 2 [34], where the roll mass $m = 0.2Kg$, the nominal air gap $e = 0.5mm$ and the force constants $\lambda_1 = \lambda_2 = 0.000005 \left[\frac{Nm^2}{A^2} \right]$; x denotes the horizon deviation of the center of the ball from its nominal position; F_1, F_2 are the magnetic forces; and i_1, i_2 are the associated currents. The dynamics of this active magnetic bearing system is described as Eq. (15) [34].

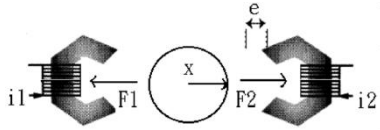


Fig.2: horizontal active magnetic bearing systems [34].

$$m\ddot{x} = F_1 - F_2 = \frac{\lambda_1 i_1^2}{(e - x)^2} - \frac{\lambda_2 i_2^2}{(e + x)^2}. \quad (15)$$

We choose the rotor position and control current as the training inputs and the rotor acceleration as the training output. 2300 training patterns generated from Eq. (15) are fed into the neural-fuzzy inference network in Fig. 1. The learning rate is set at 0.005. After training we have the following T-S fuzzy system [31],

$$\begin{aligned} R^1: & \text{If } x(t) \text{ is } T_1(-0.0025, 0.005), \\ & \text{then } \dot{X}(t) = A_1 X(t) + B_1 u(t). \\ R^2: & \text{If } x(t) \text{ is } T_2(-0.003536, 0.07497), \\ & \text{then } \dot{X}(t) = A_2 X(t) + B_2 u(t), \end{aligned} \quad (16)$$

where the system states $X(t) = [\dot{x}(t) \ x(t)]^T$ and the system inputs $u(t) = [i_1(t) \ i_2(t)]^T$; the fuzzy term set $T_i(m_i, \sigma_i)$, $i = 1, 2$, has Gaussian membership function with mean m_i and standard deviation σ_i ; the system parameters

$$A_1 = \begin{bmatrix} 0 & 55000 \\ 1 & 0 \end{bmatrix}, A_2 = \begin{bmatrix} 0 & 43000 \\ 1 & 0 \end{bmatrix}, B_1 = \begin{bmatrix} 63 & -59.6 \\ 0 & 0 \end{bmatrix}, B_2 = \begin{bmatrix} 49.9525 & -46.251 \\ 0 & 0 \end{bmatrix}.$$

According to Theorem 4, we are able to predict the steady state response of T-S fuzzy system in Eq. (13) to two sinusoidal inputs, $u_1(t) = \sin(0.3907t)$ and $u_2(t) = \sin(0.1931t)$. The sinusoidal input $u_1(t)$ and the corresponding steady state response are shown in blue color, and those to $u_2(t)$ are shown in red color. We observe that the steady state response $y_{ss}(t)$ oscillates at ± 0.001105 for $u_1(t)$ and at ± 0.001079 for $u_2(t)$.

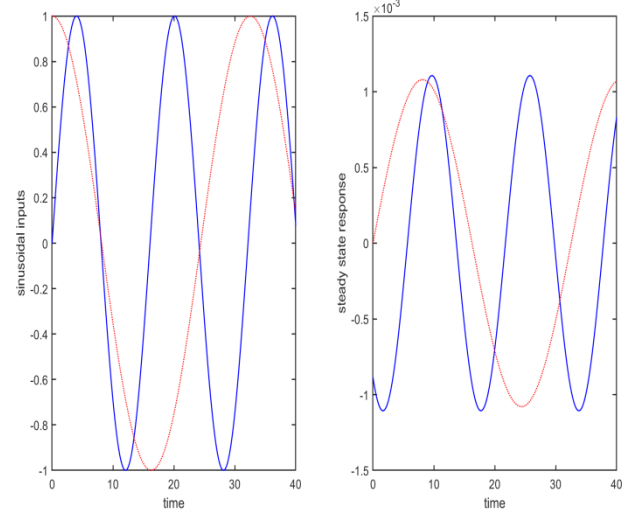


Fig. 3: steady state response $y_{ss}(t)$ for fuzzy system in Eq. (16).

■ horizontal differential-driving-mode magnetic bearings

We then consider a differential-driving-mode bearing systems in Fig. 4 [35]. One magnet is driven by the sum of bias-current and control-current and the other by the difference between these two currents. We have the dynamic equation of rotor motion in Eq. (17) [35].

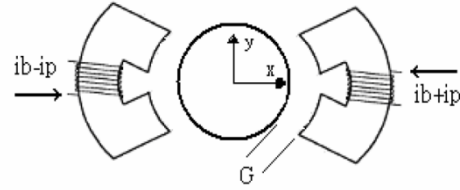


Fig.4: horizontal differential-driving-mode magnetic bearing system [35].

$$m\ddot{x} = \lambda \frac{(i_b + i_p)^2}{(G - \beta x)^2} - \lambda \frac{(i_b - i_p)^2}{(G + \beta x)^2}, \quad (17)$$

The i_p is the control current and $i_b = 0.3$ is the bias current; the rotor mass $m = 0.0126 \text{ lb} \cdot \frac{\text{sec}^2}{\text{in}}$, the nominal air gap $G = 0.02 \text{ in}$, the force constant $\lambda = 0.0186 \text{ lb} \cdot \frac{\text{in}^2}{\text{A}^2}$ and the sensitivity of the air gap to shaft displacement $\beta = 0.974$.

We also choose the rotor position and the control current as the training inputs, and the rotor acceleration as the training output. After feeding 2300 training patterns generated from Eq. (17) into the neural-fuzzy inference network in Fig. 1 with a learning rate at 0.005. We have the following T-S fuzzy system [31],

$$\begin{aligned} R^1: & \text{If } x(t) \text{ is } T_1(0, 0.2), \\ & \text{then } \dot{X}(t) = A_1 X(t) + B_1 u(t). \\ R^2: & \text{If } x(t) \text{ is } T_2(-0.4389, 0.08826), \\ & \text{then } \dot{X}(t) = A_2 X(t) + B_2 u(t), \end{aligned} \quad (18)$$

where the system states $X(t) = [\dot{x}(t) \ x(t)]^T$ and the system input $u(t) = i_p$; the fuzzy term set $T_i(m_i, \sigma_i)$, $i = 1, 2$, has Gaussian membership function with mean m_i and standard deviation σ_i ; the parameters $A_1 = \begin{bmatrix} 0 & 14000 \\ 1 & 0 \end{bmatrix}, A_2 =$

$\begin{bmatrix} 0 & 16880 \\ 1 & 0 \end{bmatrix}$, $B_1 = \begin{bmatrix} 300 \\ 0 \end{bmatrix}$, $B_2 = \begin{bmatrix} 560 \\ 0 \end{bmatrix}$. Based on Theorem 4, we have the steady state response of the T-S fuzzy system in Eq. (14) to a sinusoidal input signal $u_1(t) = \sin(0.3907t)$ and to a cosine input signal $u_2(t) = \cos(0.1931 + 0.1)$. The sinusoidal input $u_1(t)$ and the corresponding steady state response are shown in blue color, and those to $u_2(t)$ are shown in red color. We observe that the steady state response $y_{ss}(t)$ oscillates at ± 0.2143 for both signals.

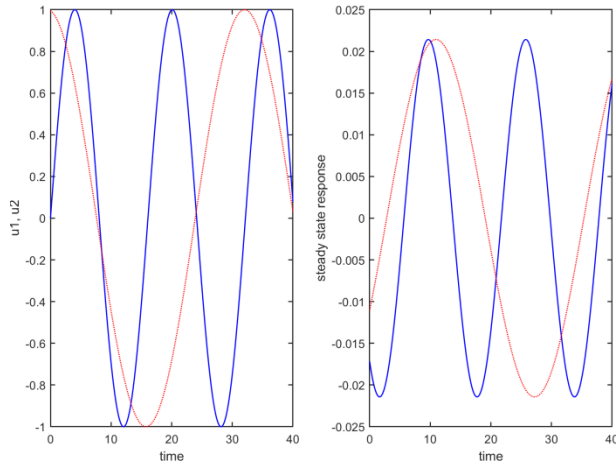


Fig. 5: steady state response $y_{ss}(t)$ for fuzzy system in Eq. (18).

4. CONCLUSION

Frequency response is used to minimize audible distortion of an audio system and to assess system stability of control systems, for example, vehicle cruise control systems. However, linear frequency domain analysis cannot apply to nonlinear systems. T-S fuzzy systems possess linear subsystems and at any time instant the dynamic behavior of entire fuzzy systems is a fuzzily blending effect of all linear subsystems. Based on this characteristic, we introduce previously proposed neural fuzzy inference network to describe system response to input signals in time domain, and then to demonstrate the feasibility and limitations of frequency domain. In the future we shall develop module-based numerical approaches to overcome the limitations of nonlinear T-S fuzzy frequency response.

5. ACKNOWLEDGMENTS

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